

1 LINEARIZATION OF AN INCREMENTAL PRINTER BY MEASUREMENTS
2 REFERRED TO A MEDIA-INDEPENDENT SENSOR CALIBRATION

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5 RELATED PATENT DOCUMENTS
6

7 Related documents are other, coowned U. S. utility-
8 patent documents hereby incorporated by reference in their
9 entirety into this document. One is in the names of Pau
10 Soler et al., attorney docket 60004608Z141, entitled "COM-
11 PENSATING FOR DRIFT AND SENSOR PROXIMITY IN A SCANNING
12 SENSOR, IN COLOR CALIBRATING INCREMENTAL PRINTERS" and la-
13 ter assigned U. S. patent application serial __/__,
14 issued as U. S. 6,____,____; another of Francesc Subirada
15 et al., attorney docket 60002868Z136, entitled "TEST-BASED
16 ADVANCE OPTIMIZATION IN INCREMENTAL PRINTING: MEDIAN,
17 SENSITIVITY-WEIGHTED MEAN, NORMAL RANDOM VARIATION" and
18 later assigned U. S. patent application serial __/__,
19 issued as U. S. 6,____,____; still another of Francesc Su-
20 birada et al., U. S. application serial 09/034,722, "SCAN-
21 NING AN INKJET TEST PATTERN FOR DIFFERENT CALIBRATION AD-
22 JUSTMENTS", issued as U. S. 6,____,____; another of Thomas
23 H. Baker et al., serial 09/183,819 entitled "COLOR-CALI-
24 BRATION SENSOR SYSTEM FOR INCREMENTAL PRINTING" and issued
25 as U. S. 6,____,____; yet another of Francis Bockman and
26 Guo Li, entitled "CONSTRUCTING DEVICE-STATE TABLES FOR
27 INKJET PRINTING", U. S. application serial 08/960,766,
28 issued as U. S. 6,____,____; and U. S. 5,796,414 of Otto
29 Sievert et al., "SYSTEMS AND METHOD FOR ESTABLISHING POSI-
30 TIONAL ACCURACY IN TWO DIMENSIONS BASED ON A SENSOR SCAN
31 IN ONE DIMENSION".
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1 FIELD OF THE INVENTION

2
3 This invention relates generally to machines and pro-
4 cedures for incremental printing of text or graphics on
5 printing media such as paper, transparency stock, or other
6 glossy media; and more particularly to calibration of a
7 sensor used in such machines and procedures for lineariz-
8 ation preparatory to printing with two or more of such
9 media.

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11
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13 BACKGROUND OF THE INVENTION

14
15 For short-run work, particularly for single copies or
16 a few copies, incremental printers are far faster and more
17 economical than printing presses. This enormous advantage
18 flows from a totally different set of approaches, tech-
19 niques and processes in the two technologies.

20 Incremental printers form colors through a set of es-
21 sentially electromechanical procedures, though chemistry
22 is important in the interaction between inks and printing
23 media. These procedures are quite different from the fun-
24 damentally optical/photochemical (and modernly also compu-
25 ter-graphics) operations used in offset printing.

26 Incremental printing does have its own limitations
27 and constraints. Such limitations can be appreciated from
28 a comparison of the methods used for defining pixels, and
29 forming colors, in the two very different technologies.

30
31 (a) Printing-press technology — Traditionally, pix-
32 els of offset negatives and plates are defined and shaded
33 by extremely high-precision — and extremely expensive —

- 1 ▪ split-millisecond timing,
- 2
- 3 ▪ an inexpensive consumable component known as a
- 4 "printhead" or (in inkjet printing) "pen", and
- 5
- 6 ▪ inks specially formulated to be amenable to ejection,
- 7 flight and deposition without physical contact be-
- 8 tween hardware and medium.
- 9

10 In incremental printing each act, or operation, of mechan-
11 ically defining a particular pixel thus serves — and in-
12 stantaneously serves — one and only one application of
13 colorant to the medium.

14 If another printed copy of the image is desired, the
15 entire array of pixels must be mechanically redefined from
16 scratch by the same hardware, the only commonality being
17 the image-data computer file that defines informationally
18 what the electromechanical hardware will later define me-
19 chanically. (As noted above, an information source is
20 present in offset work too, but not normally consulted for
21 each additional printout.)

22 Due to the extremely dynamic and transitory nature of
23 this pixel-defining and -marking process — and particu-
24 larly in view of the relatively humble and inexpensive
25 printhead that is at the crux of this process — the re-
26 sulting colorimetric tones are subject to significant
27 variation. By the same token, however, the entire process
28 at each point — being dynamic — is subject to pixel-wise
29 control, and this point-by-point control is readily ex-
30 ploited to correct or compensate for undesired variation.

31

32 (c) Colorimetric nonlinearity — In particular, the
33 variation just mentioned is often manifested in nonline-
34 arity of tonal steps — in nominally linear colorimetric

1 shadings. Linearity of tonal steps is extremely important
2 to colorimetric accuracy.

3 Linearity is important not merely to the precise per-
4 ceptible shade (e. g. lightness) of a single subtractive
5 primary printed alone, but also to the hue and chroma of
6 all complex shades formed by printing dots of the differ-
7 ent primaries mixed together. Linearity in incremental
8 printing requires, in effect, either:

- 9
- 10 (1) a very precise relationship between the size of each
11 colorant dot and the size of each pixel that such a
12 dot may occupy — or, alternatively,
13
- 14 (2) an arithmetic adjustment to each input tonal value to
15 accommodate imprecision in that relationship.
16

17 When the dot-to-pixel size relationship is correct,
18 then a nominally linear geometrical sequence of activated-
19 pixel fractions produces a similarly linear sequence of
20 actual inking fractions — without any need for arithmetic
21 adjustment. Accomplishing linearity in this way, however,
22 would be prohibitively expensive because nonlinearity can
23 arise from minute tolerances in any of a great number of
24 operating parameters.

25 These include for example the electronic timing of
26 dot-formation commands, and interactions between the
27 printing medium and the colorant; and, in inkjet work,
28 distance of inkdrop flight from printhead to printing
29 medium, nozzle size and directionality, heater chamber
30 size, and heater firing energy. The latter four factors
31 affect inkdrop volume, which in turn influences both dot
32 size and dot placement. All the parameters mentioned also
33 directly affect colorant dot coalescence with nearby dots.
34

1 (d) Linearization procedures — Hence in a practi-
2 cal, economical sense high-quality printing with incremen-
3 tal systems and methods requires actual measurement of
4 tonal-step linearity, and retention of linearization
5 correction coefficients or the like for use in printing
6 images thereafter. This kind of correction is known in
7 the art, and may be effectuated by any of various tech-
8 niques — some open-loop, others closed-loop.

9 Some such procedures are centered upon factory meas-
10 urements for each individual printer, or for an entire
11 line of printers. Others are based on measurements made
12 in the field (i. e. after distribution of the product),
13 either automatically by programmed systems in each printer
14 or by procedures prescribed for performance by human op-
15 erators of the equipment — or partly automatic, partly
16 manual.

17 All linearization procedures necessarily rely, at
18 some point in the cumulative history of the overall data,
19 whether in factory or field, upon printing and measurement
20 of a test pattern. Such measurement is followed by feed-
21 back of measured errors as correction signals to color-
22 adjusting stages in the printing system of the individual
23 printer.

24
25 It is well known in this field that results of line-
26 arization are different when a printing system is using
27 different inks, or different printing media — or both.
28 Therefore, the system linearization procedure must be re-
29 peated whenever a new set of printheads (pens, in inkjet
30 systems) is placed into service — and also whenever the
31 print media are changed.

32 The printing and measurement procedures that are
33 needed to accomplish the linearization, described above,
34 necessarily consume both ink and printing medium — as

1 well as time. Since linearization is fundamental to good
2 image quality, however, these investments of resources are
3 well spent.

4
5 (e) Linearization hardware — In the measurement
6 phases of linearization, a reliable measuring device is
7 required. This may be a high-quality colorimeter — for
8 instance a free-standing one such as mentioned in the
9 coowned U. S. patent 5,272,518 of Vincent, or a printer-
10 mounted one such as taught in another coowned patent of
11 Vincent, U. S. 5,671,059, or in the above-mentioned patent
12 document of Thomas Baker.

13 A colorimeter is or can be made direct-reading in
14 perceptual colorimetric space, such as the well-known
15 CIELAB space. Such direct perceptual readout is very fa-
16 vorable, since it is in perceptual terms that a printing
17 system ideally should be linearized.

18 Alternatively and much more economically, however,
19 the measuring device can be a simple densitometer, or even
20 a relatively crude optical sensor that is custom driven —
21 and whose output signals are specially interpreted — to
22 yield values that the Baker document terms "pseudodensito-
23 metric" measurements. Such a device is especially favora-
24 ble in a production-printer environment, for measurements
25 to be made in the field after product distribution, be-
26 cause many or most sophisticated incremental printers al-
27 ready include such a sensor for other uses.

28 In particular a simple optical sensor — often denom-
29 inated a "line sensor" — is provided for such purposes as
30 pen alignment, and other strictly positional calibrations.
31 (A representative application of such a sensor is taught
32 in the Sievert patent document mentioned earlier.) In
33 scanning printers, a line sensor ordinarily is mounted to

1 the carriage that holds the printheads and scans them back
2 and forth across the printing medium.

3 Actually for such usages a sensor need do little more
4 than distinguish dark from light. This is accordingly the
5 type of sensor that a colorimetric calibration module can,
6 in effect, inherit from the general operations of an in-
7 cremental printer.

8 The line sensor consists of a light source and an
9 electrooptical detector. The source illuminates the print
10 medium and whatever marks have been printed upon it, and
11 the detector produces an electrical signal related to the
12 light reflected from the medium and those marks. In prac-
13 tice the source is often a light-emitting diode, or in
14 better units two such diodes emitting light of different
15 colors so that the sensor can respond suitably to the sev-
16 eral subtractive primary colorants used in printing.

17
18 (f) Fine linearization with modest equipment — The
19 challenge then becomes how to infuse such a primitive
20 device with an adequately close approximation to the high-
21 quality measuring capabilities of a perceptual-reading
22 colorimeter — or, more precisely, how to do so at minimal
23 cost and complexity. It is conventional in the art of
24 incremental printing to meet this challenge by calibrating
25 the sensor itself, in perceptual terms, and storing the
26 calibration data for use whenever a linearization is to be
27 performed.

28 There have been several different overall approaches
29 to providing such a calibration of the sensor. The cali-
30 bration, at least in principle, can be performed either at
31 the factory or in the field — but factory calibration is
32 the only prior method which the present inventors know was
33 actually commercialized:

34

1 to be changed after a printer has been distributed and is
2 in the field, i. e. in an end-user's facility.

3 In any event, the calibration values were then saved
4 in the printer memory for all the machines in the product
5 line, and/or in some part of the product line carrying a
6 particular respective sensor subpopulation. In all cases,
7 separate calibration numbers were saved for each different
8 printing medium.

9
10 As indicated above, although field calibration of the
11 sensor has been possible in principle, the present inven-
12 tors are not aware of any prior commercialization of that
13 approach. If sensor calibration is performed in the
14 field, then presumably it is done whenever a new set of
15 colorants or printheads (or both) is placed in service —
16 and also whenever a different type of printing medium is
17 first placed in service.

18 Since we assume here that the printer is available
19 for sensor calibration, one field-calibration strategy is
20 to conserve printer memory space by calling for the cali-
21 bration to be performed shortly before each linearization;
22 then only one set of media data need be stored at any one
23 time.

24 An alternative strategy is to simplify the operation
25 or usage of the machine by storing many sets of media data
26 — upon acquiring such data in the field — and then call-
27 ing up a suitable set by media type, as in the factory
28 sensor-calibration case.

29
30 In any event, after sensor calibration, as noted
31 above, the system is ready to perform a linearization for
32 the inks and medium then in use. It has been natural to
33 perform such changes in calibration, like the lineariza-
34 tion, for each different printing medium because in the

1 linearization process — as also mentioned above — the
2 sensor responded differently to test patterns printed on
3 different media. In other words, the requirement to cali-
4 brate the sensor separately for each different printing
5 medium was grounded in the requirement to linearize sepa-
6 rately for each change of print medium.

7
8 (g) Drawbacks in conventional calibration — Un-
9 fortunately, regardless of which of the above-discussed
10 approaches and strategies is adopted, several problems
11 result:

12
13 First, when sensor calibration is performed in the
14 factory any media introduced by the printer manufacturer
15 after a particular printer has been distributed to an end-
16 user — and third-party media as well — are absent from
17 the media-data memory. This is a serious problem because
18 special provision must then be made for use of such media,
19 or the media are usable only without proper linearization.

20 Another serious problem is that calibration of a line
21 sensor is not strictly accurate unless it is performed
22 using the particular ink sets and printheads that will be
23 used in the linearization and subsequent printing.

24 Yet another problem is that memory storage space in
25 the printer must be dedicated to the calibration data.
26 The amount of data, however, is modest and this problem is
27 secondary.

28
29 Second, if sensor calibration is performed in the
30 field (if in fact this has been done), while this miti-
31 gates the problem of third-party and postintroduction
32 media — and as well the problem of inaccuracy due to
33 calibration without actual inks and pens to be used — it
34 does introduce other difficulties. Adoption of the first-

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1 than related to colorimetry (or even pseudodensitometry)
2 as such. This is an automatic, routine and rapid proce-
3 dure that is performed both in the field — i. e. in the
4 facilities of an end-user — and in the factory.

5 It is performed before — usually just before — op-
6 eration of each algorithm that will use the line sensor,
7 in particular just before a linearization or a sensor cal-
8 ibration. Its purpose is basically to assure that there
9 is enough optical signal on the sensor, and thereby enough
10 electrical signal from the sensor.

11 This procedure prints a color patch on white paper
12 for each ink color and calculates optimum electronics set-
13 tings (gain and offset on the signal amplifiers) for each
14 color on the given printing medium, and for the bare medi-
15 um; however, as suggested above, this calibration has no
16 direct relationship with color. For each patch and par-
17 ticularly for the bare medium, the LED current is raised
18 until adequate signal appears — most typically eight or
19 sixteen steps on the analog-to-digital converter ("ADC")
20 — and then until the sensor signal saturates; and then
21 the current is lowered slightly to establish suitable
22 dynamic range.

23 The purpose of this procedure is only to optimize the
24 ADC dynamic range, and improve the electronic signal-to-
25 noise ratio, for a given printing medium and ink set. For
26 purposes of this document, this procedure is not a "cali-
27 bration" and will be called a "dynamic-range adjustment".

28
29

30 (i) Conclusion — As this discussion suggests, limi-
31 tations in efficiency of preparing an incremental printer
32 system for use continue to impede achievement of uniformly
33 excellent inkjet printing that is within the constraints
34 of acceptability to product buyers, owners and operators.

1 Thus important aspects of the technology used in the field
2 of the invention are amenable to useful refinement.

3
4
5
6 SUMMARY OF THE DISCLOSURE

7
8 The present invention introduces such refinement. In
9 its preferred embodiments, the present invention has several
10 aspects or facets that can be used independently, although
11 they are preferably employed together to optimize
12 their benefits.

13 In preferred embodiments of a first of its facets or
14 aspects, the invention is an automatic method of linearizing
15 a color printing system, for forming images on plural
16 printing media. The method uses measurements made with an
17 optical sensor that is onboard the system.

18 The method includes the step of referring to a single
19 calibration of the sensor; this calibration is used in
20 common for substantially all the plural media. This single
21 calibration, however, is with respect to exclusively a
22 single one of the plural media. (In other words, when the
23 calibration is actually performed, it is performed with
24 respect to just one of the media.)

25 The method also includes the step of using the sensor,
26 as calibrated by the single common calibration, to
27 colorimetrically linearize the system for printing with
28 each of plural colorants on any one medium, of the plural
29 media. (In other words, the calibration although performed
30 with respect to just one printing medium is then
31 applied more broadly for linearization as to any of the
32 media.) Yet another step is thereafter maintaining the
33 system as thus linearized for printing on that one medium.

1 using the calibrated onboard sensor to colori-
2 metrically measure the ramps to determine
3 actual tonal levels, and
4
5 for each of the plural colorants respectively,
6 determining corrections for subsequent ap-
7 plication at each nominally specified tonal
8 level to linearize actually printed tonal
9 levels.
10
11 If this basic preference is in use, then some subsidiary
12 or auxiliary preferences also are applicable.
13 In one such subsidiary preference, the using step
14 includes measuring an unprinted area of the first medium
15 as a reference white point for the linearizing. In anoth-
16 er, the ramp-printing substep includes printing each re-
17 spective ramp with negligible hue-angle variation along
18 the ramp.
19 In still another such subsidiary preference — par-
20 ticularly for a sensor that incorporates at least one il-
21 luminator — to stabilize illumination in the sensor, the
22 using substep comprises operating the at least one illumi-
23 nator continuously before and during measurement of the
24 ramps.
25 One further basic preference is that the said single
26 calibration include plural subcalibrations for plural ink
27 types respectively. In this case it is further preferred
28 that the plural ink types respectively include pigment
29 inks and dye inks.
30
31
32
33 In preferred embodiments of its second major indepen-
34 dent facet or aspect, the invention is an automatic method

1 of linearizing and then using a color printing system, to
 2 form a color image on any one of plural printing media.
 3 The method is based upon measurements made with an optical
 4 sensor that is onboard the system.

5 The method includes the step of referring to a single
 6 calibration of the sensor. The single calibration is with
 7 respect to exclusively a single one of the plural media —
 8 but is used in common for substantially all the plural
 9 media.

10 The method includes the step of using the sensor, as
 11 calibrated by the single common calibration, to colorimet-
 12 rically linearize the system for printing with each of
 13 plural colorants on any one medium, of the plural media.
 14 Another included step is thereafter using the system with-
 15 out further sensor calibration to form a properly colori-
 16 metrically linearized image on any different one medium,
 17 of the plural media.

18 The foregoing may represent a description or defini-
 19 tion of the second aspect or facet of the invention in its
 20 broadest or most general form. Even as couched in these
 21 broad terms, however, it can be seen that this facet of
 22 the invention importantly advances the art.

23 In particular, the advantage arising from this facet
 24 of the invention is complementary to the advancement noted
 25 above for the first aspect of the invention. For this
 26 second aspect, the benefits of economical calibration are
 27 extended from the context of the calibration procedure it-
 28 self to the context of using a printer system to produce
 29 images of fine color quality.

30

31 Although the second major aspect of the invention
 32 thus significantly advances the art, nevertheless to
 33 optimize enjoyment of its benefits preferably the inven-
 34 tion is practiced in conjunction with certain additional

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1 which are parts of its context — and thereby to more par-
2 ticularly claim the invention.)

3
4 Also included are second processor portions for per-
5 forming a second program. This program operates the prin-
6 ter, and the sensor as calibrated by the single common
7 calibration, to colorimetrically linearize the system for
8 printing with each of plural colorants on any one medium,
9 of such plural media.

10 In addition the printer includes a memory for there-
11 after maintaining linearization data, for the printer as
12 thus linearized, for printing on said any one medium, of
13 the plural media. It will be understood that these reci-
14 tations mean that the single common sensor calibration
15 serves in linearization for printing on any one, not just
16 some particular specially selected one, of the plural
17 media.

18 The foregoing may represent a description or defini-
19 tion of the third aspect or facet of the invention in its
20 broadest or most general form. Even as couched in these
21 broad terms, however, it can be seen that this facet of
22 the invention importantly advances the art.

23 In particular, this facet of the invention is in es-
24 sence a hardware manifestation that is particularly advan-
25 tageous for calibration of the sensor in the field. As
26 explained earlier, a benefit of using just one sensor cal-
27 ibration for all media is that field calibration is not
28 necessary; however, it may still be desirable in event the
29 sensor must be changed, or if the system is to be used
30 with newly introduced inks.

31 In the latter case, field calibration avoids the
32 necessity of downloading information into the printer from
33 the WorldWide Web or otherwise. Benefits of this third

1 aspect of the invention essentially parallel those of the
2 first and second aspects discussed earlier.

3
4
5
6 In preferred embodiments of its fourth major indepen-
7 dent facet or aspect, the invention is an automatic method
8 of calibrating an optical sensor and using the sensor to
9 linearize a color printing system that forms images on
10 plural printing media. This method includes the step of
11 deriving a single sensor calibration from ideal properties
12 of color inks, without making any optical measurement us-
13 ing the sensor.

14 It also includes the step of referring to the derived
15 single calibration, used in common for substantially all
16 the plural media; and furthermore the step of using the
17 sensor as calibrated by the single common calibration to
18 colorimetrically linearize the system for printing with
19 each of plural colorants on any one medium, of the plural
20 media.

21 Another step is thereafter maintaining the system, as
22 thus linearized, for printing on the one medium. The
23 foregoing may represent a description or definition of the
24 fourth aspect or facet of the invention in its broadest or
25 most general form.

26 Even as couched in these broad terms, however, it can
27 be seen that this facet of the invention importantly ad-
28 vances the art. In particular, this facet of the inven-
29 tion offers an extremely rapid and generalized way to get
30 sensor-calibration data without any of the drawbacks of
31 resorting to measurements.

32
33 Although the fourth major aspect of the invention
34 thus significantly advances the art, nevertheless to

1 optimize enjoyment of its benefits preferably the inven-
2 tion is practiced in conjunction with certain additional
3 features or characteristics. In particular, the preferen-
4 ces introduced above as to each aspect of the invention
5 are applicable to all the other facets too, including this
6 fourth aspect.

7
8
9 All of the foregoing operational principles and
10 advantages of the present invention will be more fully
11 appreciated upon consideration of the following detailed
12 description, with reference to the appended drawings, of
13 which:

14
15
16
17 BRIEF DESCRIPTION OF THE DRAWINGS

18
19 Fig. 1 is a graph of local contrast ratio for magenta
20 ink, using a Panasonic® blue LED and a Hewlett Packard
21 amber LED (as well as a TAOS® TSL251 receptor);

22 Fig. 2 is a like graph but using instead two Hewlett
23 Packard LEDs — one bluish-green and another red-orange
24 (and the TAOS unit too);

25 Fig. 3 is a group of four graphs showing perceptual-
26 color-space parameters corresponding to absolute and local
27 contrast ratios, as derived on the basis of ideal inks —
28 without measurement, in keeping with the above-mentioned
29 fourth main facet of the invention; and

30 Fig. 4 is a block diagram, highly schematic, repre-
31 senting hardware (including programmed circuitry) in a
32 preferred embodiment of the invention.

1 DETAILED DESCRIPTION
2 OF THE PREFERRED EMBODIMENTS
3
4

5 1. SENSOR CALIBRATION FOR ALL MEDIA IN COMMON
6

7 In prior incremental-printer products and procedures,
8 as discussed in the "Background" section of this document,
9 it has been conventional to use a line sensor and to pro-
10 vide a separate calibration of that sensor for use with
11 each different printing medium. The present inventors are
12 aware of prior Hewlett Packard commercial products that
13 operated in this way, based upon factory calibrations com-
14 mon to a whole product line — and saved in the printer
15 memory.

16 The media-dependent sensor calibrations (i. e. ap-
17 propriate to particular media respectively) were to be
18 invoked in preparation for each relinearization of the
19 printing system — and this was possible only for media
20 known to the printer manufacturer at the time of product
21 distribution. These calibrations were also limited in
22 accuracy because of the manufacturing tolerances in ink
23 sets and printheads actually placed in service in the
24 field.

25 The present invention eliminates both these handicaps
26 — the limitation to media known and recognized in advance
27 by the printer manufacturer, and also the ink-set/print-
28 head accuracy limitation. This is accomplished by cali-
29 brating in the field.
30

31 If any commercial products previously employed field
32 line-sensor calibration that was media dependent, the in-
33 vention also eliminates the relatively onerous dual proce-
34 dure (requirement to perform both sensor recalibration and

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1 to the basic $L^*a^*b^*$ formulas, it can be clearly seen that
2 if there are two different reference whites, in tristimu-
3 lus coordinates (X_0, Y_0, Z_0) and (X_1, Y_1, Z_1) there are also two
4 corresponding $L^*a^*b^*$ systems.

5 To pass from one system to the other, the X, Y, Z sys-
6 tem can be used to connect the two. This can be done by
7 back-solving the equations for each case.

8 To instead demonstrate that if a tone ramp is line-
9 arized in one system it is also linearized in the other,
10 an effective algebraic strategy is to characterize small
11 increments $\Delta L, \Delta a, \Delta b$ in the $L^*a^*b^*$ system in terms of
12 the corresponding X, Y, Z variables. When this is done and
13 the X, Y, Z expressions worked through for L^* in particular,
14 it will be found that a change in the reference white only
15 scales the L^* values by a constant.

16 This in turn implies that in the L^* dimension line-
17 arization can be performed independently of the reference
18 white that is used — i. e., the linearization is media-
19 independent. This clearly indicates that L^* is a desira-
20 ble parameter for use in linearizing a color ramp.

21 One meaningful reason to object to using L^* is that
22 it has a smaller range, as compared with a^* or b^* , for a
23 particular colorant. This is in fact importantly so in
24 the case of yellow.

25 Although the proof is somewhat more complicated and
26 less strictly accurate, a closely analogous scaling-by-a-
27 constant and media independence can be shown for the a^*
28 and b^* dimensions. Based on such a demonstration, pre-
29 ferred embodiments of the present invention use b^* for
30 linearization of yellow.

31 These conclusions have been stated in terms of line-
32 arization. As suggested above, however, the same conclu-

1 mentioned earlier; for present purposes, however, the
2 intense concern as to stability reflected in that document
3 is typically not required. Another preferred form of pat-
4 tern layout and scan procedure is introduced in the first
5 of the two earlier-mentioned patent documents of Francesc
6 Subirada et al.

7 Each of the ramps is printed using a different one of
8 the subtractive primary colorants available in the system.
9 Refining the linearization for the particular combination
10 of ink and printing medium, however, first requires a cal-
11 ibration of the line sensor.

12 13 14 3. LINE-SENSOR CALIBRATION

15
16 There are fundamentally three ways in which this can
17 be provided using the present invention:

- 18
19 ■ a sensor calibration for the entire product line can
20 be developed at the factory, measuring the response
21 of a sizable number of the sensors and finding a sui-
22 table representative relation — such as a mean, or a
23 weighted mean, etc. — and storing the sensor cali-
24 bration data in a nonvolatile memory of each printer
25 in the line;
- 26
27 ■ a sensor calibration for the particular sensor in
28 each individual printer can be developed at the fac-
29 tory, measuring the response of that sensor only —
30 and again storing calibration information in a mem-
31 ory, but only a memory of that individual printer; or
- 32
33 ■ a sensor calibration for the particular sensor can be
34 developed in the field, most typically in the end-

- 1 ▪ linearization must be performed for each combination
2 of ink and printing medium;
- 3
- 4 ▪ sensor calibration, according to the present inven-
5 tion, must be performed for each ink set but not for
6 each printing medium;
- 7
- 8 ▪ the linearization process requires that the sensor
9 calibration be done first;
- 10
- 11 ▪ the sensor calibration process requires an already
12 linearized, printed test pattern;
- 13
- 14 ▪ such a test pattern cannot be printed, on the partic-
15 ular printer to be linearized, before the sensor cal-
16 ibration is done.

18 Therefore it is necessary to use a previously printed test
19 pattern — made either with some other printer that was
20 well linearized at the time, or with the same printer ear-
21 lier when it was linearized. For instance, a preprinted
22 test pattern may be supplied from the factory, with the
23 printer; however, such targets may be subject to degrada-
24 tion, particularly if not kept sealed away from air and
25 out of the light.

26 If the sensor response itself is linear, then it can
27 be shown mathematically that a sensor calibration made
28 using one print medium is good for all other print media
29 of equal or lesser lightness. In practice, however, even
30 if the sensor response itself is not linear — in particu-
31 lar, if the output is equal to the input raised to some
32 power that is not equal to one (unity) — then such non-
33 linearity can be subsumed within the sensor calibration.

1 This is true only if the nonlinearity is not overly
2 strong, e. g. if a nonunity exponent is close to unity.
3 If a stronger or more complicated nonlinearity is present,
4 it may interfere with orderly interpolation.

5
6 More specifically, whether for linearization or for
7 sensor calibration, the line-sensor readings are first
8 used to find normalized values. The present inventors use
9 the terms "absolute contrast ratio" ("ACR") for the norma-
10 lized black-ink ramp measurement signals, and "local con-
11 trast ratio" ("LCR") for the chromatic ink ramps.

12 Derivation of ACR and LCR is shown in sections 6 and
13 7 below. (These variable names are used in the present
14 document somewhat differently than in some of the other
15 patent documents mentioned earlier.)

16
17 If it is sensor calibration that is being performed,
18 then nothing has just been printed; rather, the sensor has
19 measured known-linear patterns of known tonal values. The
20 ACR and LCR (normalized sensor readings, as above) are
21 compared with known correct perceptual readings of a
22 CIELAB colorimeter.

23 Again, the departures are effectively inverted to
24 develop conversion factors (or terms). The system can
25 then rely upon sensor readings as equivalent to CIELAB
26 values, when performing linearization as described below.

27 Preferably the conversion numbers are stored in the
28 printer memory in the form of lookup tables, for quick ap-
29 plication to input tonal values in each plane — most usu-
30 ally with one interpolation stage. If desired, however,
31 it is possible to instead develop a correction function,
32 for instance using spline techniques, for use in calculat-
33 ing CIELAB values from the sensor-signal normalized ACR
34 and LCR numbers.

1 Once again, according to the present invention, just
2 one sensor calibration does suffice for all media. On the
3 other hand, regardless of which form of correction is
4 preferred, it is helpful to have one set of sensor-cali-
5 bration values for each type of ink.

6 In principle a single calibration may be made to suf-
7 fice for all inks as well. For future convenience, howev-
8 er, because the character of inks to be introduced in the
9 future cannot be foretold as well as the character of me-
10 dia to be introduced in the future — and because interac-
11 tion of the sensor with different inks is usually somewhat
12 more complex than with different media — it is not ad-
13 vised to attempt such a strategy.

14 15 16 4. SYSTEM LINEARIZATION

17
18 On the other hand, if it is linearization that is
19 being performed, the ACR and LCR numbers from the sensor
20 are translated into perceptual (preferably CIELAB) values.
21 True colorimetric linearity of the printed test patterns
22 can then be evaluated.

23 Measured departures from desired linearity are next
24 in effect inverted to develop linearizing adjustments for
25 application to tonal values expressed in image data. When
26 these adjustments are applied, the printing system thereby
27 is actually instructed to produce tonal values slightly
28 higher or lower than truly desired.

29 In other words, in effect deliberate errors are in-
30 troduced. This is done, however, in the knowledge that
31 these deliberate errors and the nonlinearities present in
32 the system will counteract one another, thereby producing
33 correct tones.

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1 The linearization includes generation of, most pref-
2 erably, nine-bit transfer functions and also error-diffu-
3 sion thresholds (analogously to the procedure introduced
4 in the patent document of Bockman and Li mentioned earli-
5 er). These intermediates are applied to color signals
6 just before or during halftoning — below the printer-lan-
7 guage level, and invisible to conventional operations in
8 that language.

9 This last point is true whether the printer-language
10 pipeline in use is for instance PostScript®, HPGL or RTL.
11 Accordingly the same linearization can be used in any such
12 printer language pipeline, a capability which represents
13 another favorable innovation.

14 A separate linearization should be performed for each
15 combination of ink and media. It is not suggested that
16 only one linearization can suffice for all media, or for
17 all inks.

18 Starting without a prelinearized system, linearity
19 measurements suggest a mean nonlinearity of roughly 3 dE,
20 and maximum of about 7 dE. (The units "dE" represent a
21 well-known measure of small distances in three-dimensional
22 perceptual color space.) Starting instead from a preline-
23 arized system, these values can be reduced to approximate-
24 ly 1 dE average, and 2 to 3 dE maximum.

25
26

27 5. FURTHER LINE-SENSOR CALIBRATION DETAILS

28

29 Practice of the present invention does not require
30 any deep familiarity with theoretical analysis of measure-
31 ment systems, or with colorimetric principles, although
32 the present inventors have performed such analysis and are
33 familiar with those principles. One particularly advanta-
34 geous characteristic of the invention is that it can be

1 straightforwardly practiced on the basis of only the gen-
2 eral descriptions presented in this document.

3 Some generalities found through the inventors' analy-
4 sis and system design, and useful in obtaining perspective
5 for practice of the invention, are these:

- 6
- 7 ■ The line sensor can be characterized as a linear
8 system.

9 This result is of central importance to the
10 present invention, for it is what enables sensor cal-
11 ibration with just one single printing medium to
12 serve for all media. As suggested above, small or
13 smoothly varying nonlinearities in the sensor re-
14 sponse are tolerable — and in fact simply become
15 part of the overall variation for which the sensor
16 calibration accounts.

- 17
- 18 ■ The typical sensor is a broadband device.

19 Preferred sensors for use in this field are sen-
20 sitive over the entire visible spectrum, though not
21 uniformly. A representative line sensor in a printer
22 has maximum response in the infrared.

- 23
- 24 ■ Economical sensor illuminants are ordinarily LEDs,
25 currently a pair: one amber, one blue.

26 These sources together provide an adequate ap-
27 proximation to white light — for maximum response in
28 sensing the relative tonal values of the subtractive-
29 primary and black inks ordinarily used in incremental
30 printing. Operating the two sources simultaneously
31 is useful for best stability.

32 Such simultaneous operation, however, does re-
33 quire high-quality electronics (including an analog-
34 to-digital conversion stage with very high dynamic

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- 1 ■ Adequate sensor stabilization requires accommodating
2 warmup of the LEDs.

3 In particular, the illumination they emit — and
4 accordingly the reflection from the test pattern, and
5 the corresponding signal generated by the sensor —
6 varies with temperature. Temperature affects both
7 the overall light-emission efficiency and the spec-
8 tral distribution (including the peak wavelength) of
9 each diode. To bring these factors under control,
10 before beginning actual measurements the LEDs should
11 be operated for a period of time necessary to stabi-
12 lize their temperature.

13 14 15 6. DEFINITION AND DETERMINATION OF A. C. R. VALUES

16
17 The previously mentioned ACR and LCR, as these are
18 used in the present document, are useful intermediate
19 variables that conveniently relate raw data from the line
20 sensor to perceptual measures of tonal values in the test-
21 pattern ramp for each colorant plane. As suggested earli-
22 er, these perceptual measures may be acquired for use to
23 indicate the ability of either:

- 24
25 ■ the sensor, to read a standard, correct test pattern
26 accurately — in perceptual terms; or
27
28 ■ the printer, to make a correct test pattern.

29
30 In either case, the ACR is a normalized form of the
31 raw data readings from the sensor. For a reference
32 "white" (for example, the bare unprinted printing medium),
33 the maximum ACR will be that of the medium itself (100%
34 ACR) and the minimum will occur when all power for all

1 wavelengths in the illumination is absorbed (0% ACR) by an
2 absolute black colorant.

3 ACR accordingly can be defined, for a particular col-
4 or tone measured by the sensor, as a quotient of reflected
5 light power P_{ABS} vs. the incident power P_{INC} — again, tak-
6 ing into account all the desired spectrum for a wavelength
7 range:

$$8 \quad ACR = \frac{P_{\text{REF}}}{P_{\text{INC}}} .$$

10 For normalization purposes, however, the power reflected
11 from a particular color tone patch should first be correc-
12 ted for an offset that is due to the sensor yielding a
13 nonzero reading when the light reaching it can be assumed
14 to be zero:

$$16 \quad P_{\text{REFL}} = P_{\text{PATCH}} - P_K .$$

18 The incident power P_{INC} is a special case of this same ex-
19 pression, obtained when there is no printed patch, so that
20 reflection is maximum — the value P_{MED} received from the
21 bare unprinted printing medium:

$$23 \quad P_{\text{INC}} = P_{\text{MED}} - P_K .$$

25 Here P_{INC} is represented simply as the maximum possible
26 value of reflected light power, which is to say the dif-
27 ference between the sensor readings of power reflected
28 from the print medium P_{MED} and from an absolute black col-
29 orant P_K .

30 Inserting into the expression given above for the
31 ACR:

$$33 \quad ACR = \frac{P_{\text{PATCH}} - P_K}{P_{\text{MED}} - P_K} .$$

1 Taking the sensor measurement signals \underline{M} as proportional
2 (within small nonlinearities as mentioned earlier) to the
3 power values \underline{P} , the ACR can therefore be expressed direct-
4 ly in terms of the sensor signals \underline{M} .

5 The various proportionality factors implicit in the
6 relationship between \underline{M} and \underline{P} — such as in particular the
7 effective area over which the light is collected through
8 the sensor field of view — cancel out, leaving the con-
9 clusion that ACR can be measured directly for any triad of
10 light reflected from (1) a particular patch, (2) paper
11 "white" and (3) absolute black:

$$ACR = \frac{M_{PATCH} - M_K}{M_{MED} - M_K}.$$

12
13
14
15 As a practical matter, however, the line-sensor meas-
16 urement signals \underline{M} indicated here are advantageously taken
17 making several samples of the sensor signal — ordinarily
18 on the order of ten samples — and averaging them. As
19 suggested earlier, it is important that the average sat-
20 isfy thermal-stabilization criteria.

21 22 23 7. DEFINITION AND DETERMINATION OF L. C. R. VALUES

24
25 The concept of ACR, as shown in the previous section,
26 is analogous to having an absolute-referenced measurement.
27 Such a derivation is directly applicable to black, because
28 black always absorbs almost all of the visible spectrum,
29 and in particular absorbs all the LED power independently
30 of the spectral balance of that power.

31 This assumption fails for the chromatic colorants
32 CMY, whose absorption depends strongly on the spectral
33 balance of the LEDs. Referred to the absorption of abso-
34 lute black, the value varies depending on the spectrum of

the diodes, and so disrupts the line-sensor independence that is pursued here.

There cannot exist one lookup table that relates sensor readings to CIELAB for all possible sensors. The dependence, moreover, can be affected by spectral variation among LEDs of different standard types (Fig. 1) and some alternative types (Fig. 2).

The illustrations exhibit variation in the 100%-of-magenta ACR, amounting to a divergence of roughly eight percent in this concrete case. Self-warming spectral variation still further complicates the response for the chromatic color inks.

For robustness relative to this LED spectral variation for all the colors other than black, LCR can be defined analogously to ACR but taking as reference 100% of the ink color rather than 100% of absolute black. Thus with $M_{N \text{ MAX}}$ the maximum sensor response for color-plane "N" (e. g. one of the chromatic colorants CMY, or in some systems the dilute colorants cm, etc.), the LCR is:

$$LCR = \frac{M_{\text{PATCH}} - M_{N \text{ MAX}}}{M_{\text{MED}} - M_{N \text{ MAX}}}.$$

It can be shown that the ACR measurements are the fundamental basis for dynamic closed-loop color, using the invention, while LCR is just a derivative from it. Familiarity with the derivation, however, is not necessary to effective practice of the present invention. The relation can be written:

$$LCR_{\text{ACTUAL}} = 1 - \frac{1 - ACR_{\text{ACTUAL}}}{1 - ACR_{\text{MAXIMUM}}}.$$

In this expression, ACR_{actual} is found from the previous expression for ACR in terms of P_{PATCH} or M_{PATCH} — but evaluated for an intermediate tonal value of one of the chromatic-

color inks — while ACR_{MAXIMUM} is seen in the previous expression for ACR, evaluated for 100% of that color.

8. SENSOR CALIBRATION TABLES FROM IDEAL INKS

Procedures for sensor calibration based on actual measurements have been described above, particularly in subsections 1, 3, and 5 through 7 of this Detailed Description. Those procedures are particularly useful in obtaining sensor-to-CIELAB conversions that are fully adapted to the spectral behavior of actual inks, as distinguished from ideal colorants.

Achieving such a full adaptation to real-world inks is a main reason for preparing tables specific to each ink. It is possible, however, to establish fairly workable sensor-to-'LAB conversions based on ideal relationships.

The idea is to establish a relationship between the ACR and LCR variables and the $L^*a^*b^*$ system. For a particular primary (e.g. magenta), if a path is defined from that color to white, then it is possible to map, for that specific color, a relationship between the ACR and the $L^*a^*b^*$ of that color ramp.

As an example, this task has been performed using Adobe Photoshop® graphics program. Color ramps were defined going from white to each primary KCMY, and then the $L^*a^*b^*$ "measurements" were taken for each ramp patch using the same Photoshop program.

The resulting values constitute the sensor-to-LAB tables for each color. Data (Fig. 3) in these tabulations, although of course inaccurate because they do not account at all for true spectral properties of actual inks, are usable.

1
2 9. HARDWARE AND PROGRAM IMPLEMENTATION
3

4 As the invention is amenable to implementation in, or
5 as, any one of a very great number of different printer
6 models of many different manufacturers, little purpose
7 would be served by illustrating a representative such
8 printer. If of interest, however, such a printer and some
9 of its prominent operating subsystems can be seen illus-
10 trated in several other patent documents of the assignee,
11 Hewlett Packard — such as for example the previously men-
12 tioned document of Thomas Baker, which particularly illus-
13 trates a large-format printer-plotter model.
14

15 (a) General mechanics and electronics — In some
16 such representative printers, a cylindrical platen 241
17 (Fig. 4) — driven by a motor 242, worm and worm gear
18 (shown as encircling the platen 241) under control of
19 signals from a digital electronic processor 71 — rotates
20 to drive sheets or lengths of printing medium 4A in a
21 medium-advance direction. Print medium 4A is thereby
22 drawn out of a supply of the medium and past the marking
23 components that will now be described.

24 A pen-holding carriage assembly 220 carries several
25 pens, as illustrated, back and forth across the printing
26 medium, along a scanning track — perpendicular to the
27 medium-advance direction — while the pens eject ink. For
28 simplicity's sake, only four pens are illustrated; how-
29 ever, as is well known a printer may have six pens or
30 more, to hold different colors — or different dilutions
31 of the same colors as in the more-familiar four pens. The
32 medium 4A thus receives inkdrops for formation of a de-
33 sired image.
34

1 A very finely graduated encoder strip 233, 236 is ex-
2 tended taut along the scanning path of the carriage assem-
3 bly 220 and read by a very small automatic optoelectronic
4 sensor 237 to provide position and speed information 237B
5 for one or more microprocessors 71 that control the opera-
6 tions of the printer. One advantageous location (not
7 shown) for the encoder strip is immediately behind the
8 pens.

9 A currently preferred position for the encoder strip
10 233, 236 (Fig. 4), however, is near the rear of the pen
11 carriage — remote from the space into which a user's
12 hands are inserted for servicing of the pen refill car-
13 tridges. For either position, the sensor 237 is disposed
14 with its optical beam passing through orifices or trans-
15 parent portions of a scale formed in the strip.

16 The pen-carriage assembly 220, 220' is driven in
17 reciprocation by a motor 231 — along dual support and
18 guide rails (not shown) — through the intermediary of a
19 drive belt 235. The motor 231 is under the control of
20 signals 231A from the processor or processors 71.

21 Preferably the system includes at least four pens
22 holding ink of, respectively, at least four different col-
23 ors. Most typically the inks include yellow Y, then cyan
24 C, magenta M and black K — in that order from left to
25 right as seen by the operator. As a practical matter,
26 chromatic-color and black pens may be in a single printer,
27 either in a common carriage or plural carriages.

28 Also included in the pen-carriage assembly 220, 220'
29 is a tray carrying various electronics. Fig. 4 most
30 specifically represents a system such as the Hewlett Pac-
31 kard printer/plotter model "DesignJet 2000CP", which does
32 not include the present invention. These drawings, how-
33 ever, also illustrate certain embodiments of the inven-
34 tion, and — with certain detailed differences mentioned

below — a printer/plotter that includes preferred embodiments of the invention.

Before further discussion of details in the block diagrammatic showing of Fig. 4, a general orientation to that drawing may be helpful. This diagram particularly represents preferred embodiments of one previously discussed apparatus aspect of the invention.

Conventional portions of the apparatus appear as the printing stage 220 . . . 251, and 4A, discussed above, and also the final output-electronics stage 78 which drives that printing stage. This final-output stage 78 in turn is driven by a printmasking stage 75, which allocates printing of ink marks 218, 219 as among plural passes of the carriage 220, 220' and pens across the medium 4A.

Also generally conventional are a nonvolatile memory 77, which supplies operating instructions 66 (many of which are novel and implement the present invention) for all the programmed elements; an image-processing stage 73, rendition-and-scaling module 74; and color input data 70 seen at far left in the diagram. The data flow as input signals 191 into the processor 71.

Features particularly related to the apparatus aspect of the invention appear in the upper and upper-central region of the diagram as element 72, and elements 80 through 89; these will be detailed below. Given the statements of function and the diagrams presented in this document, a programmer of ordinary skill — if experienced in this field — can prepare suitable programs for operating all the circuits.

The pen-carriage assembly is represented separately at 220 when traveling to the left 216 while discharging ink 218, and at 220' when traveling to the right 217 while discharging ink 219. It will be understood that both 220

1 (e. g. held in a ROM 77 and for distribution 66 to other
2 components), or both; and may comprise application-spe-
3 cific integrated circuitry. Combinations of these may be
4 used instead.

5
6 The novel features appear primarily in the color-
7 calibrating processing portions 72 — which include a two-
8 stage interpretive system 79, 83. Also novel in this con-
9 text is a module 80 for controlling the final output stage
10 78 and printing stage 220 . . . 251, and 4A, to generate a
11 test pattern for interpretation by the second (lineariza-
12 tion) stage 83.

13
14 (b) Sensor-to-perceptual calibration — In first op-
15 eration of the calibrating portions 72, the system scans
16 the line sensor — which is another small optical sensor
17 251 that also rides on the carriage — over a preprinted
18 test pattern known to be linear. This sensor is detailed
19 in the previously mentioned patent document of Soler (see
20 Fig. 5 and discussion in that document).

21 The result is a signal stream 65 from the sensor 251
22 to the first stage 79, which calibrates the sensor (as
23 distinguished from linearizing the printing system). This
24 stage 79 includes a front end 62 that reads and preinter-
25 prets the known-linear test pattern — and as earlier ex-
26 plained does so for only one single printing medium.

27 Based on the interpreted data, the main section 63 of
28 the first-stage calibration module 79 determines conver-
29 sion factors at multiple points — or a spline-like func-
30 tion, as mentioned earlier. Resulting calibration data
31 are stored in a memory 64; as a practical matter, this
32 memory may be part of the nonvolatile memory 77.

33 Calibration of the sensor is thus completed. The
34 calibration data remain in the memory 64 for use until the

1 sensor requires recalibration due to changing of the sen-
 2 sor, or its aging, or accumulated ink spray on its optical
 3 window, or other events that may be suspected to modify
 4 the actual response of the sensor and so require a new
 5 calibration.

6
 7 (c) Printing-system linearization — Next, for actu-
 8 al linearization of the printing system — now relying on
 9 the already-calibrated sensor — the control module 80
 10 provides signals 81 to the final output stage 78, inducing
 11 that stage to operate the printing stage 220 . . . 251,
 12 and 4A, to generate a new test pattern. This test pattern
 13 is not known to be linear, and in fact the purpose of
 14 printing it is specifically to determine its nonlineari-
 15 ties and a transfer function required to essentially elim-
 16 inate them.

17 Unlike the single test pattern used for the sensor
 18 calibration described above, the linearization test pat-
 19 tern now under discussion should be printed on each dif-
 20 ferent printing medium that is to be used in the printer.
 21 Of course it is not necessary if the operator is not con-
 22 cerned with tonal linearity in some particular project.

23 It also is not necessary to perform such printing and
 24 linearization for all the printing media at one time.
 25 Rather, these operations can be performed when a particu-
 26 lar type of print medium is about to be used for the first
 27 time, or after this type of medium has not been used for a
 28 long while — and also if the printheads or inks have been
 29 changed.

30 After the new test pattern has been printed, then
 31 again the sensor 251 is scanned over the pattern as in the
 32 sensor calibration — but resulting data 82 from the sen-
 33 sor now flow to the second, linearization stage 83 of the
 34 calibration module 72. Here the data are interpreted 84

1 in an analogous manner to that in earlier module 62, but
 2 the interpretive calculations are aimed not at conversion
 3 factors for use of the sensor but rather at determining
 4 errors of linearization in the pattern.

5 From those errors, the next submodule 85 develops a
 6 linearization profile, or transfer function, that will
 7 later be used to adjust input color data to achieve print-
 8 out linearity. Still within the processor 71 and at the
 9 output stage of its calibrating unit 72, this lineariza-
 10 tion submodule 85 transmits the adjustment data 89 into
 11 the previously mentioned nonvolatile memory 77 for storage
 12 in a transfer-function memory bank 86.

13 In this process, one or more of various forms of the
 14 transfer-function information 89 — whether in the form of
 15 coefficients for use in a formula, or in the form of a
 16 lookup table — are then stored in their particular dedi-
 17 cated portion 86 of the memory 77. The transfer-function
 18 information is retrieved from that memory bank 86 and pas-
 19 ses 87 into the color-adjustment module 76, whenever nee-
 20 ded to guide the operation of that module in preparing the
 21 input data 70 for later transformations 74, 75, 78 and
 22 thereby for eventual printing in the printing stage.

23
 24
 25
 26 The above disclosure is intended as merely exemplary,
 27 and not to limit the scope of the invention — which is to
 28 be determined by reference to the appended claims.